

Potential theory

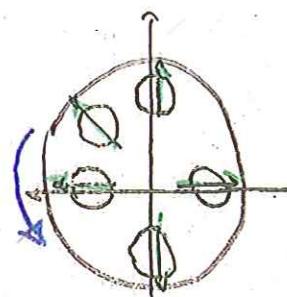
Requirements: stationary, no rotation
2-dimensional (planar)
incompressible, steady

rotation free: $\bar{\omega} = 0$

$$\vec{v} \cdot \vec{\omega} = \frac{1}{2} \nabla \times \vec{v}^2 = \frac{1}{2} \left(\frac{\partial v_y}{\partial x} - \frac{\partial v_x}{\partial y} \right) = 0$$

2-dimensional flow: $\omega_{xy} = \frac{\partial v_y}{\partial x} = 0$

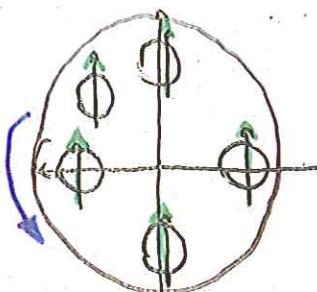
$$\rightarrow \omega_z = \frac{1}{2} (v_x - v_y) = \frac{1}{2} \left(\frac{\partial v_x}{\partial y} - \frac{\partial v_y}{\partial x} \right) = 0$$



rotational flow

[Example 1.1] $\text{rot}(\text{grad } \phi) = 0$

stationary flow
⇒ potential flow



Potential function

If $\omega_z = 0 \rightarrow$ A function ϕ exists with the

property $\vec{v} = \vec{\nabla} \phi \rightarrow (u) = \left(\frac{\partial \phi}{\partial x}, \frac{\partial \phi}{\partial y} \right)$

$$\text{Potential} \Rightarrow u = \frac{\partial \phi}{\partial x}; \quad v = \frac{\partial \phi}{\partial y}$$

→ Continuity (2-D, steady, incompressible)

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = \vec{\nabla} \cdot \vec{v} = 0 \Rightarrow \Delta \phi = 0$$

$$\Rightarrow \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = 0$$

Laplace equation of
the potential function

Linear differential equation

⇒ The principle of superposition is applicable

If ϕ_1, ϕ_2 are solutions of the equation,
then $C_1 \phi_1 + C_2 \phi_2$ and $C_1 \phi_1 + C_2 \phi_2$ are

also solutions

$$\text{Stream function: } u = \frac{\partial \psi}{\partial y}; \quad v = -\frac{\partial \psi}{\partial x}$$

$$\psi = 0 \rightarrow \nabla^2 \psi = \Delta \psi = 0$$

$$\frac{\partial \psi}{\partial x} = \frac{\partial \psi}{\partial y}; \quad \phi_1 = -\frac{\partial \psi}{\partial x} \rightarrow \phi \text{ and } \psi \text{ are perpendicular}$$

ϕ = const \rightarrow lines of constant potential

γ = const \rightarrow streamlines

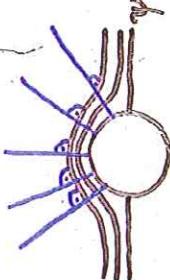
ϕ and γ are used to describe flow fields and flow around bodies.

The contour is provided by a special stream line
 \Rightarrow The velocity vector is parallel to the wall

the wall

But: Wall no-slip condition cannot be fulfilled
(frictionless + rotation free)

\rightarrow Drag forces and viscous stresses cannot be determined



complex potential function
complex stream function

$$\tilde{F}(z) = \int w dz = \phi(x, y) + i\psi(x, y)$$

$$\Rightarrow \text{Laplace-equation} \left(\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} \right) + i \left(\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right) = 0$$

$$\bar{w} = u - iv = \frac{d\tilde{F}}{dz}$$

Singularities:

Parallel flow:

$$\tilde{F}(z) = (u_\infty - i v_\infty) z = \phi + i\psi$$

$$\phi = u_\infty x + v_\infty y$$

$$u = u_\infty, v = v_\infty$$

Streamlines



Source, sink:

$$\tilde{F}(z) = \frac{E}{2\pi} \ln z = \phi + i\psi$$

$$\phi = \frac{E}{2\pi} \ln r, \quad \psi = \frac{E}{2\pi} \varphi$$

Complex velocity

$$w = u + iv$$

$$u = \frac{E}{2\pi} \frac{x}{x^2 + y^2}, \quad v = \frac{E}{2\pi} \frac{y}{x^2 + y^2}$$



Source sink

Conjugate complex velocity

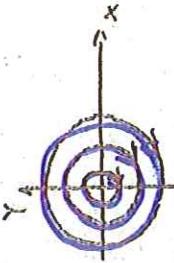
$$\bar{w} = u - iv$$

$$\tilde{F}(z) = \frac{\pi}{2\pi} i \ln z$$

Vortex:

$$\phi = -\frac{\pi}{2\pi} \arctan \frac{y}{x}$$

$$u = \frac{\pi}{2\pi} \frac{y}{x^2 + y^2}$$

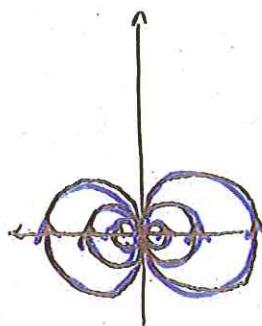


↓ pole, double

$$\tilde{F}(z) = \frac{u_0}{z}$$

$$\phi = -\frac{\ln y}{x^2 + y^2}$$

$$u = -\frac{2xy}{x^2 + y^2}$$



Superposition of
a source and a sink

$$\text{usually: } m = \frac{M}{2\pi}$$

$$\Rightarrow F(z) = \frac{M}{2\pi z}$$

Corner flow:

$$\tilde{F}(z) = \frac{a}{n} z^n$$

$$n \in \mathbb{R}$$

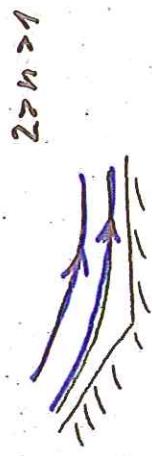
$$a \in \mathbb{C}$$

$$\phi = \frac{a}{n} \pi \cos(n\varphi)$$

$$q = \frac{a}{n} \pi \sin(n\varphi)$$

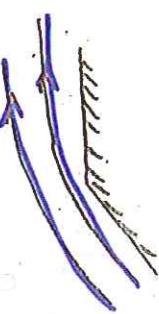
$$\text{acute angle} \quad n > 1$$

$$\text{concave}$$



$$n \geq 2$$

$$\text{concave}$$



$$1 > n > \frac{1}{2}$$

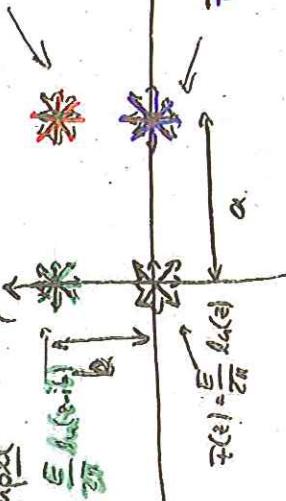
$$\text{concave}$$

Singularities have their center in the origin
of the coordinate system

→ Displacement

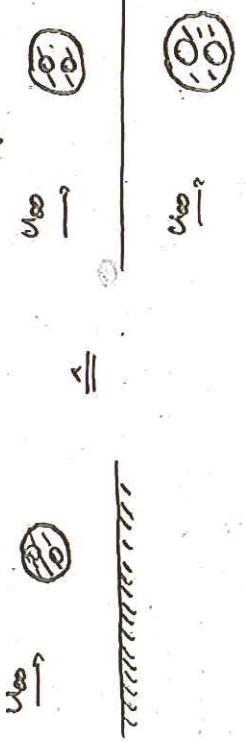
$$\text{For } \frac{E}{2\pi} h (z-a-i b)$$

Example



$$F(z) = \frac{E}{2\pi} h (z-a-i b)$$

- Streamlines of cells monitoring



- Usually, the contours are presented by the stagnation streamlines

• locate the stagnation point ($\alpha = \nu = 0$): x_S, y_S

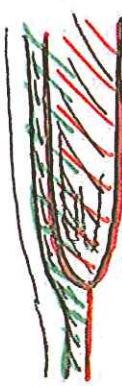
• determine if it the stagnation point!

• sketch the streamlines

$$\psi_k(x, y) = \psi_{in}(x_S, y_S) = \text{const.}$$

- Streamlines do not intersect

→ each streamline can represent a body contour. In this case usually $\alpha_0 \neq 0$



- Bernoulli's equation is valid

$$p_0 = p_\infty + \frac{1}{2} \rho (v_\infty^2 + v_0^2) = p + \frac{1}{2} \rho (\alpha^2 + r^2) = \text{const}$$

$$\text{Compress } \gamma_p = \frac{p - p_\infty}{\frac{1}{2} \rho v_\infty^2} = \frac{\frac{1}{2} \rho V^2}{\frac{1}{2} \rho v_\infty^2} = 1 - \frac{V^2}{a_\infty^2}$$

- 14.5 A planar flow is described by the stream function $\psi = (\frac{U}{L})xy$. In $x_{ref} = 0, y_{ref} = 1 \text{ m}$ the pressure is $p_{ref} = 10^5 \text{ N/m}^2$.

$$U = 2 \text{ m/s} \quad L = 1 \text{ m} \quad \rho = 10^3 \text{ kg/m}^3$$

- a) Proof, if the flow has a potential.

Determine

- b) the stagnation points, the pressure coefficient, and the lines of constant total velocity

- c) the velocity and the pressure at $x_1 = 2\text{m}, y_1 = 2\text{m}$,

- d) the coordinates of a particle at $t = 0.5\text{s}$ if it passes at $t = 0$ the point x_1, y_1 ,

- e) the pressure difference between these two points.

- f) Sketch the streamlines.

Sketch of the flow field

- stagnation points - stagnation streamline

- asymptotic streamlines for

$$x, y \rightarrow \infty ; \quad x, y \rightarrow 0$$

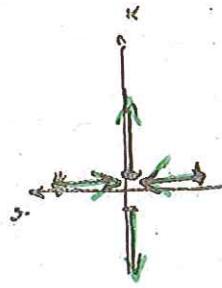
- flow direction

Stagnation points : $\bar{v} = 0$: $u_i = v_i = 0$

$$u = \frac{u}{L} x ; \quad v = -\frac{u}{L} y \rightarrow (x_s, y_s) = (0, 0)$$

Additionally: $u = 0$ on the y -axis

$v = 0$ on the x -axis



Stream lines : $\gamma = \text{const}$

$$\gamma = \frac{u}{L} x y = \text{const}$$

$$\rightarrow \gamma = \frac{u}{L} \text{const.} \quad \frac{1}{x} = \frac{c}{y} \quad \text{for } x \neq 0$$

$$x = \frac{L}{u} \text{const.} \quad \frac{1}{y} = \frac{c}{x} \quad \text{for } y \neq 0$$

→ Hyperbola

Stagnation point streamline

$$u_{sp} = \frac{u}{L} \times_{sp} \gamma_{sp} = 0 \quad | \text{ depended on the problem}$$

- $u = 0 \rightarrow x = 0 \quad \text{or} \quad y = 0$
- x -axis and y -axis are stagnation streamline

$$u = \frac{u}{L} x ; \quad v = -\frac{u}{L} y$$

$$u > 0$$

$$v < 0$$

$$v > 0$$

$$u < 0$$

$$v < 0$$

$$v > 0$$

$$u > 0$$

$$v > 0$$

$$u < 0$$

$$v < 0$$

$$v > 0$$

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$$u < 0$$

$$v < 0$$

$$v > 0$$

$$u > 0$$

$$v < 0$$

$$v > 0$$

$$u < 0$$

$$v < 0$$

$$v > 0$$

a) Given shear function $\psi = \frac{u}{L} xy$

$$\phi \text{ exists, if } \bar{\omega} = 0$$

Planar flow - 2-dimensional $\rightarrow \omega_x = \omega_y = 0$

$$\omega_z = \frac{1}{2} \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right)$$

$$u = \frac{\partial \psi}{\partial x} = \frac{u}{L} x \rightarrow \frac{\partial u}{\partial y} = 0$$

$$v = -\frac{\partial \psi}{\partial x} = -\frac{u}{L} y \rightarrow \frac{\partial v}{\partial x} = 0 \quad \left\{ \begin{array}{l} \omega_z = 0 \\ \text{the flow is irrotational} \end{array} \right.$$

and the potential exists

Exists \rightarrow Computation of ϕ

$$1) U = \frac{\partial \phi}{\partial x} \rightarrow \phi = \int u dx + f_1(y) + C_1$$

$$2) V = \frac{\partial \phi}{\partial y} \rightarrow \phi = \int v dy + f_2(x) + C_2$$

$$1) \phi(x, y) = \frac{u}{L} \frac{x^2}{2} + f_1(y) + C_1$$

$$2) \phi(x, y) = -\frac{u}{L} \frac{y^2}{2} + f_2(x) + C_2$$

Computation of f_1 and f_2

$$\frac{u}{L} \frac{x^2}{2} + f_1(y) + C_1 = -\frac{u}{L} \frac{y^2}{2} + f_2(x) + C_2$$

$$\frac{u}{L} \frac{x^2}{2} + f_1(y) + C_1 = -\frac{u}{L} \frac{y^2}{2} + f_2(x) + C_2$$

$$f_1(y) = -\frac{u}{L} \frac{y^2}{2} \quad ; \quad f_2(x) = \frac{u}{L} \frac{x^2}{2} ; \quad C_1 = C_2 = C$$

Complex potential $\tilde{\psi}(z)$

$$\tilde{\psi}(z) = \tilde{\psi}(x+iy) = \phi(x, y) + i\tilde{\psi}(x, y)$$

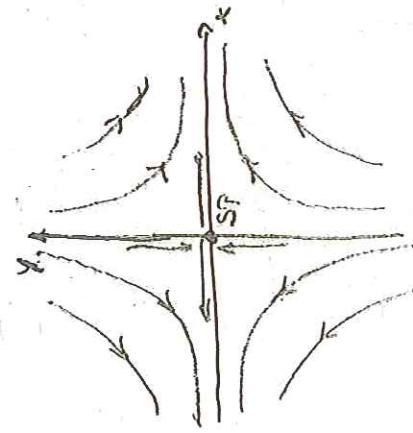
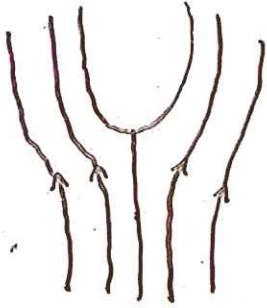
$$= \frac{u}{2L} (x^2 - y^2) + i \frac{u}{L} xy$$

$$= \frac{u}{2L} (x^2 + 2ixy - y^2)$$

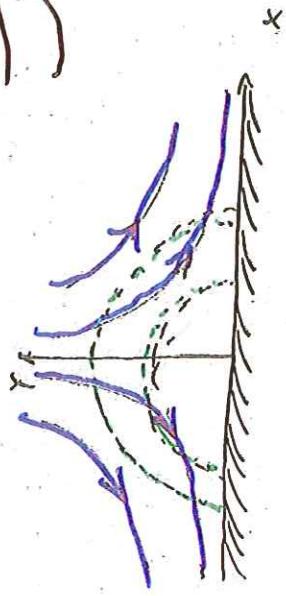
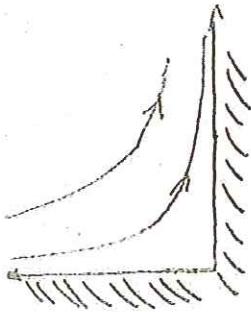
$$1) \phi(x, y) = \int \frac{u}{L} x dx + f_1(y) + C_1$$

$$2) \phi(x, y) = \int -\frac{u}{L} y dy + f_2(x) + C_2$$

$$= \frac{u}{2L} \frac{y^2}{2}$$



90° - corner flow



Corner stagnation point flow

$$\frac{P - P_{\text{atm}}}{\frac{\rho}{2} V_{\infty}^2} = \lambda - \frac{U_x^2 + U_y^2}{U_{\infty}^2}$$

$$C_p = \frac{P - P_{\text{atm}}}{\frac{\rho}{2} U_{\infty}^2} = \lambda - \frac{U_x^2 + U_y^2}{U_{\infty}^2}$$

$$U_x = \frac{U}{L} x \quad \left\{ \begin{array}{l} C_p = \lambda - \frac{x^2 + y^2}{x_{\infty}^2 + y_{\infty}^2} \\ U_y = -\frac{U}{L} y \end{array} \right.$$

lines of constant velocity

$$|\vec{V}| = \sqrt{U_x^2 + U_y^2} = \text{constant}$$

$$= \sqrt{\left(\frac{U}{L} x\right)^2 + \left(-\frac{U}{L} y\right)^2} = \sqrt{\left(\frac{U}{L}\right)^2 x^2 + y^2}$$

circle with the radius $R = \frac{U L}{U}$

$\frac{2\pi}{L}$

14.4 The complex stream function is given

$$F(z) = \frac{2u_\infty}{3\sqrt{L}} z^{\frac{3}{2}} + \frac{E}{2\pi} \ln(z)$$

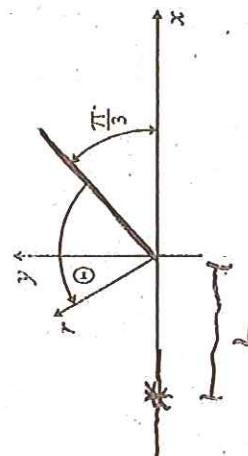
Given: L, u_∞

Determine

- the potential $\phi(r, \theta)$ and the stream function $\psi(r, \theta)$.
- the components of the velocity v_r, v_θ .
- the constant E such that a stagnation point is at $(x = -L, y = 0)$.
- the equation that describes the contour $r_k(\theta)$.

Hints:

$$\begin{aligned} z &= x' + iy' = re^{i\theta} \\ v_r &= \frac{\partial \phi}{\partial r} = \frac{1}{r} \frac{\partial \psi}{\partial \theta}, \quad v_\theta = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = -\frac{\partial \psi}{\partial r} \end{aligned}$$



$$e^{i\theta} = \cos \theta + i \sin \theta$$

$$\frac{3}{2}\theta$$

$$\begin{aligned} \text{a)} \quad \bar{T}(z) &= \frac{2}{3} \frac{u_\infty}{\sqrt{L}} z^{\frac{3}{2}} + \frac{E}{2\pi} \ln z - \underbrace{i\theta}_{i\theta} \\ &= \frac{2}{3} \frac{u_\infty}{\sqrt{L}} r^{\frac{3}{2}} e^{i\frac{3}{2}\theta} + \frac{E}{2\pi} (L r + L e^{-i\theta}) \end{aligned}$$

$$\begin{aligned} \phi(r, \theta) &= \Re(\bar{T}(z)) = \frac{2}{3} \frac{u_\infty}{\sqrt{L}} r^{\frac{3}{2}} \cos\left(\frac{3}{2}\theta\right) + \frac{E}{2\pi} L r + \\ \psi(r, \theta) &= \Im(\bar{T}(z)) = \frac{2}{3} \frac{u_\infty}{\sqrt{L}} r^{\frac{3}{2}} \sin\left(\frac{3}{2}\theta\right) + \frac{E}{2\pi} L \end{aligned}$$

$$\text{b)} \quad V_r(r, \theta) = \frac{\partial \phi}{\partial r} = u_\infty \sqrt{\frac{r}{L}} \cos\left(\frac{3}{2}\theta\right) + \frac{E}{2\pi r}$$

$$V_\theta(r, \theta) = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = -u_\infty \sqrt{\frac{r}{L}} \sin\left(\frac{3}{2}\theta\right) + \frac{E}{2\pi r}$$

c) stagnation point at $(x = -L, y = 0) \rightarrow (r = L, \theta = \frac{\pi}{2} - \theta_0)$

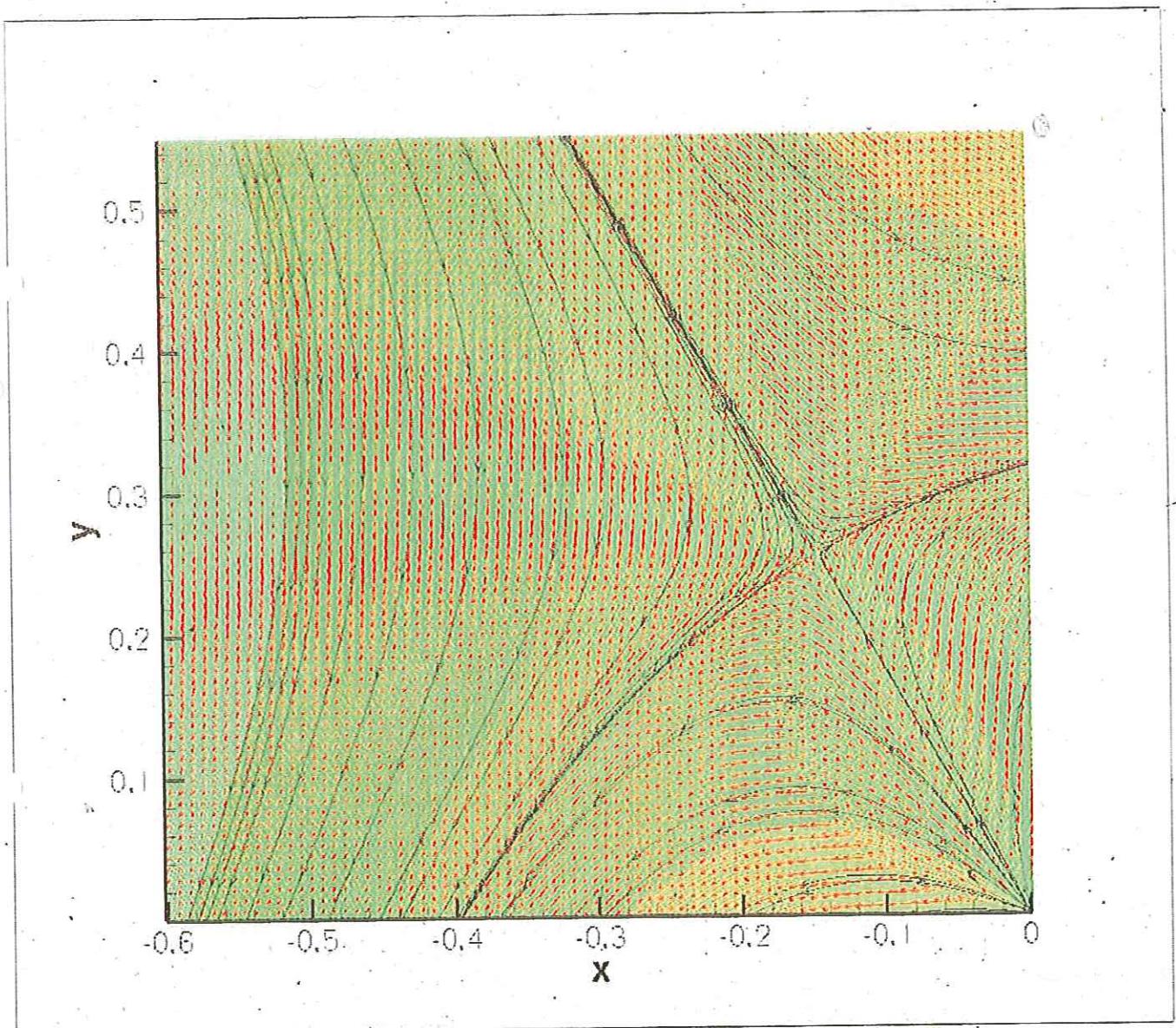
$$V_\theta = -u_\infty \sqrt{\frac{L}{r}} \sin\left(\frac{3}{2}\theta\right) = 0$$

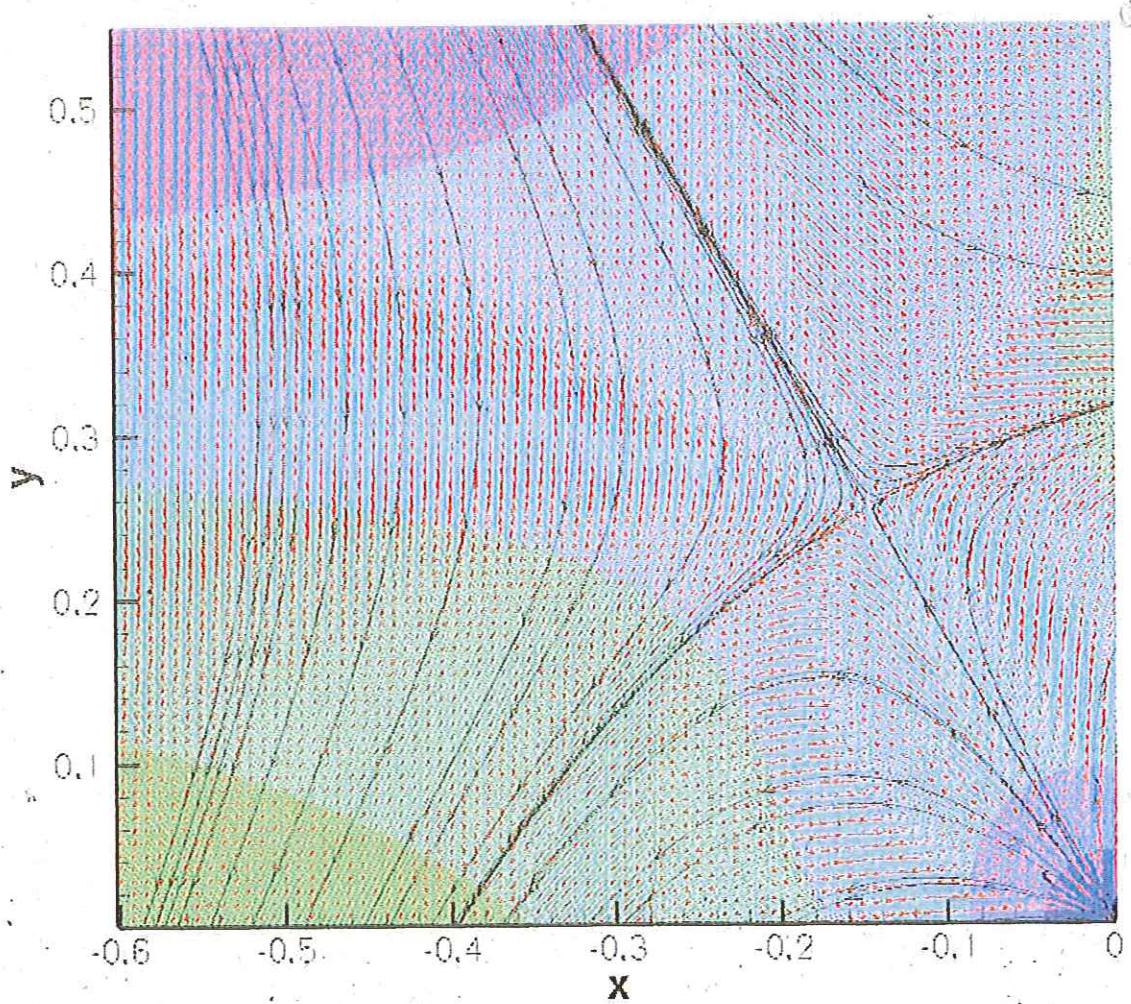
$$V_r = u_\infty \sqrt{\frac{L}{r}} \cos\left(\frac{3}{2}\theta\right) = 0 \rightarrow \frac{E}{2\pi r} = 0 \rightarrow E = 2\pi u_\infty L$$

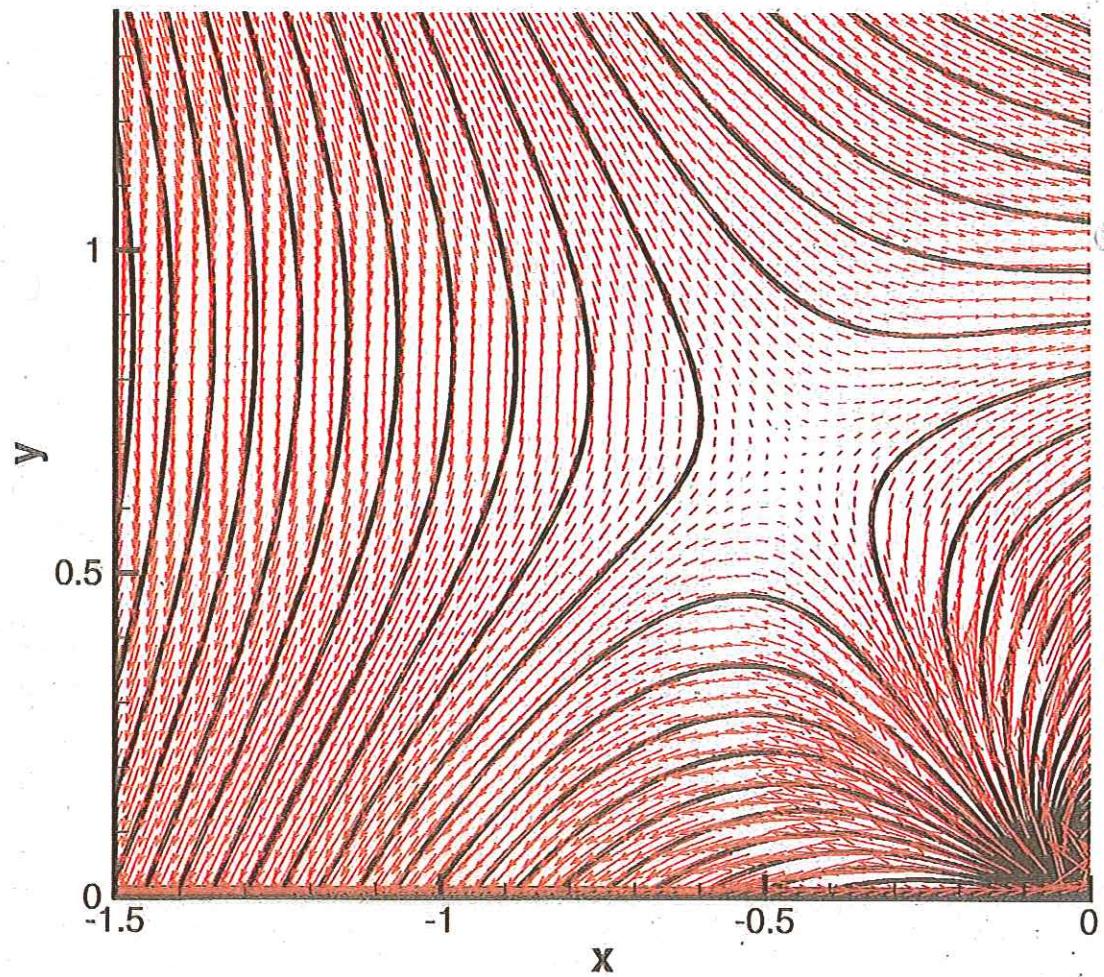
$$\text{d)} \quad \psi_{sp} = \frac{\overline{E}}{2\pi} \cdot \frac{2}{3} \frac{u_\infty}{\sqrt{L}} = \frac{E}{3} = \frac{2}{3} \pi u_\infty L = 2f_L$$

$$\frac{2}{3}\pi u_\infty L = \frac{2}{3} \frac{u_\infty}{\sqrt{L}} r^{\frac{3}{2}} \sin\left(\frac{3}{2}\theta\right) + u_\infty L \theta$$

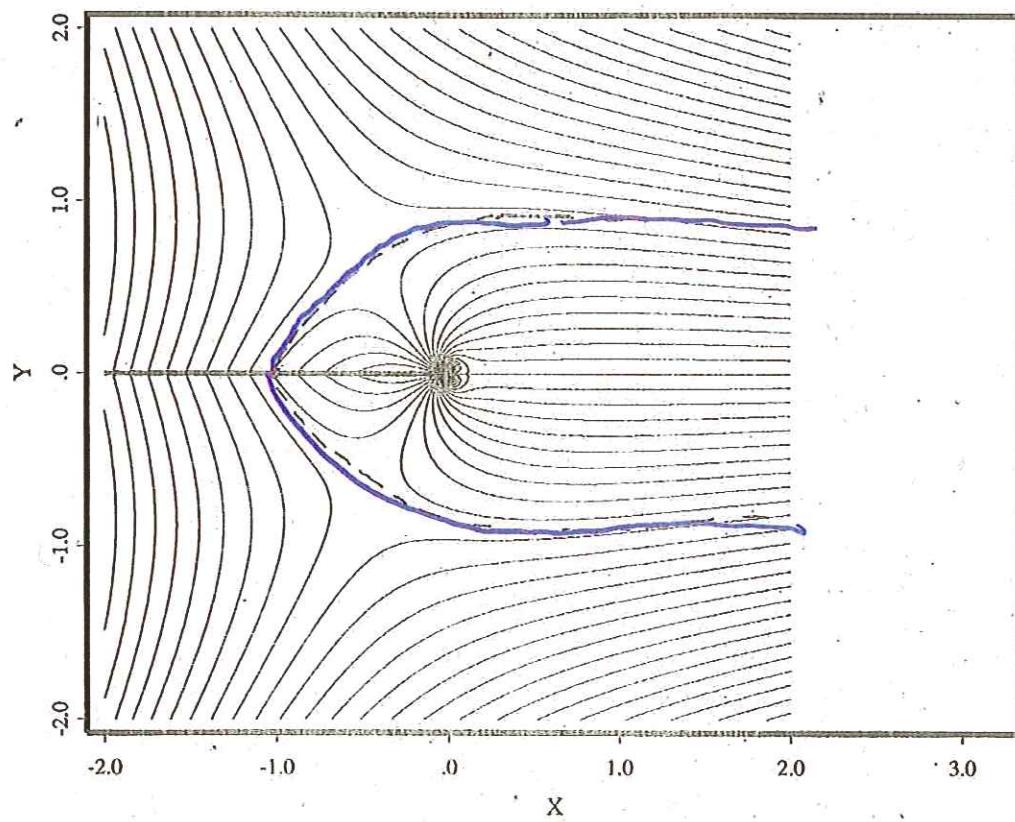
$$\rightarrow \tau_L(\theta) = L \cdot \left(\frac{\pi - \frac{2}{3}\theta}{\sin \frac{3}{2}\theta} \right)^{\frac{3}{2}}$$



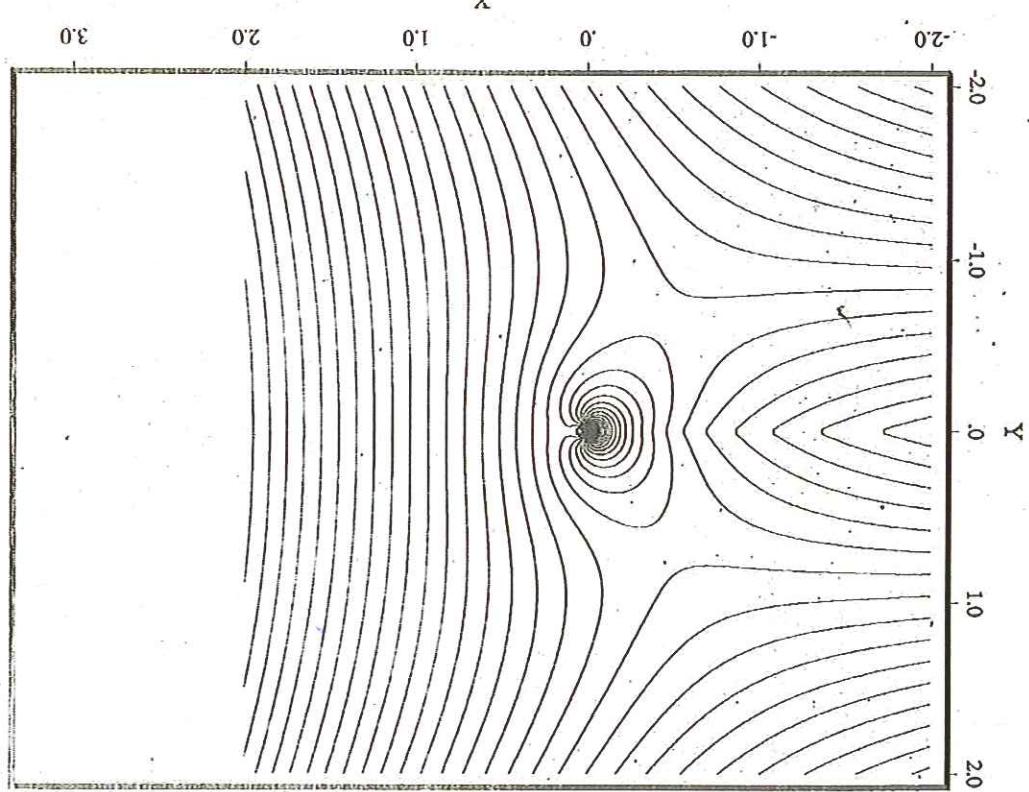




STROMFUNKTION

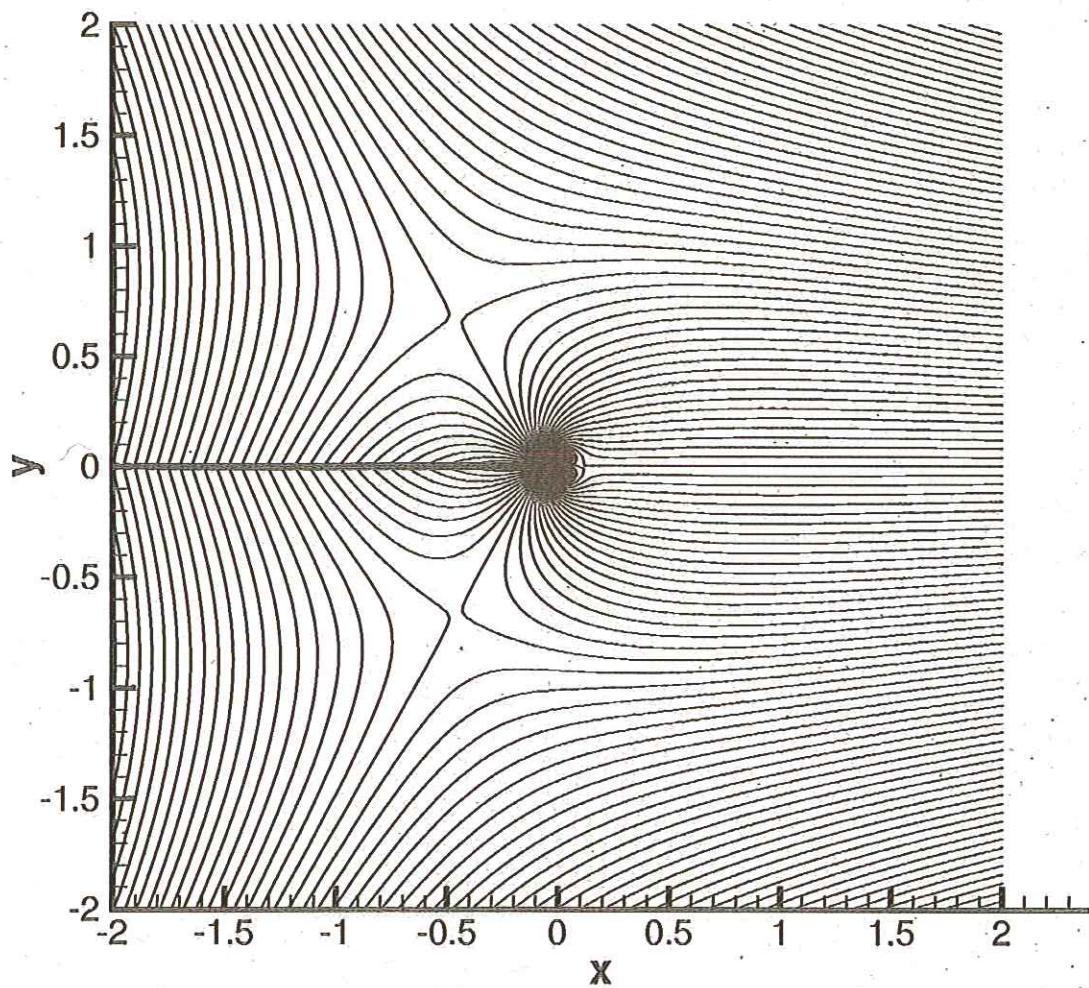


X

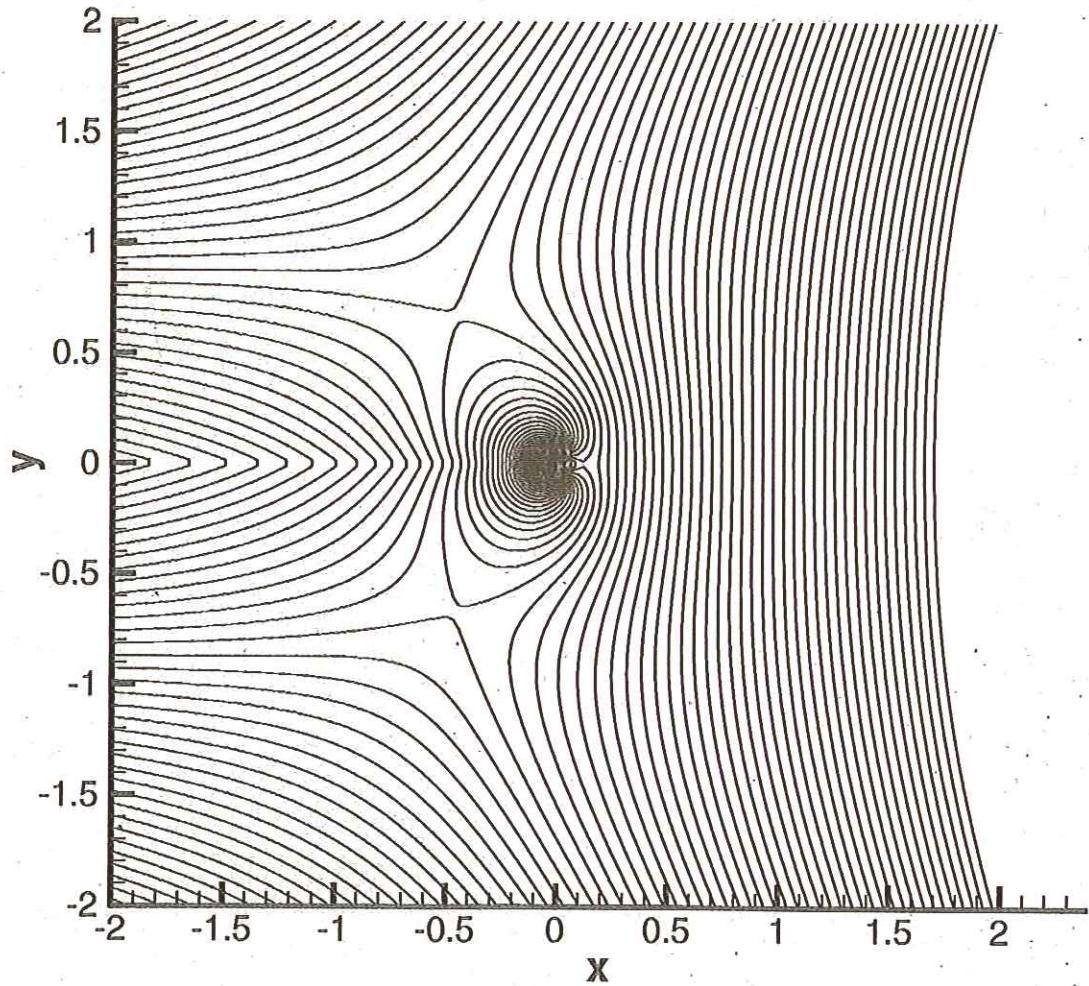


POTENTIAL

Stromlinien



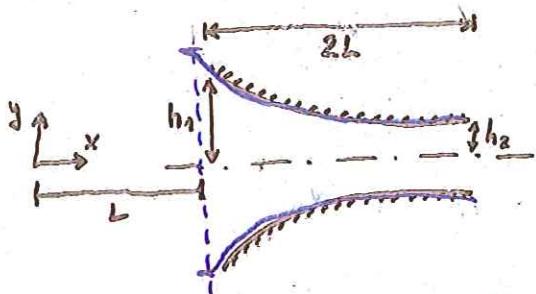
Potentiallinien



The stream function for a flow of an incompressible fluid through a planar nozzle

is given: $\Psi(x, y) = \frac{y}{h(x)} \cdot M_{\infty} \cdot L$

given: $M_{\infty}, L, B, h_1 = L, h_2 = \frac{1}{3}L$



a) Determine the shape $h(x)$ of the nozzle such that the flow can be described by the potential theory.

b) Determine the velocity distribution $u(x, y)$ and $v(x, y)$ and the volume flow.

1 prerequisite: $\omega \stackrel{!}{=} 0 \Rightarrow \nabla^2 \psi \stackrel{!}{=} 0$ with $m = \frac{\partial \Psi}{\partial y}$ and $v = -\frac{\partial \Psi}{\partial x}$

$$\Rightarrow \frac{\partial^2 \Psi}{\partial x^2} + \frac{\partial^2 \Psi}{\partial y^2} \stackrel{!}{=} 0 \quad \frac{\partial^2 \Psi}{\partial y^2} = 0$$

$$\Rightarrow \frac{\partial^2 \Psi}{\partial x^2} \stackrel{!}{=} 0 = \frac{\partial}{\partial x} \left(y M_{\infty} L \frac{\partial}{\partial x} \left(\frac{1}{h(x)} \right) \right)$$

$$\Rightarrow \frac{\partial}{\partial x} \left(-y M_{\infty} L \cdot \frac{h'(x)}{h^2(x)} \right) \stackrel{\text{inner derivative}}{=} 0$$

$$\Rightarrow \frac{d}{dx} \left(\frac{h'(x)}{h^2(x)} \right) = 0$$

$$\Rightarrow \text{integrate twice: } -\frac{1}{h(x)} = C_1 x + C_2$$

$$\text{B.C.: } x=L, h=L \Rightarrow -\frac{1}{L} = C_1 \cdot L + C_2$$

$$x=3L, h=\frac{1}{3}L \Rightarrow -\frac{3}{L} = 3C_1 \cdot L + C_2$$

$$\left. \begin{array}{l} C_2 = 0, C_1 = -\frac{1}{L^2} \\ \Rightarrow h(x) = \frac{L^2}{x} \end{array} \right\}$$

6) $m = \frac{\partial \Psi}{\partial y}; v = -\frac{\partial \Psi}{\partial x}$ with $\Psi = \frac{M_{\infty}}{L} xy$

$$\Rightarrow m = M_{\infty} \frac{x}{L} \quad \text{and} \quad v = -M_{\infty} \frac{y}{L}$$

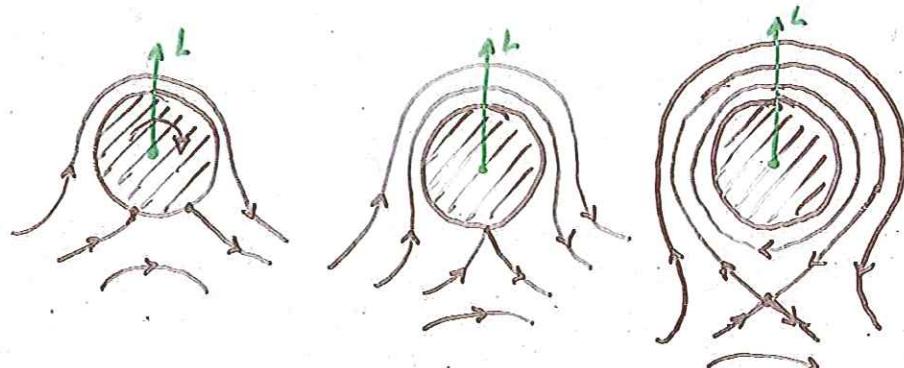
$$\dot{Q} = \Psi(y=h) - \Psi(y=-h) \Big|_{x=L} \Rightarrow \dot{Q} = (h_1 + h_2) B \cdot M_{\infty} = 2 M_{\infty} L B$$

Rotating cylinder: → force in lateral direction
 like the lift force on an airfoil
 → potential theory can be used to describe airfoil flows

$$\text{cylinder: } F(z) = M_{00}z + \frac{M}{2\pi z}$$

$$\text{rotating cylinder: } F(z) = M_{00}z + \frac{M}{2\pi z} + i \frac{\Gamma}{2\pi} \ln z$$

$$\text{with } M = 2\pi R^2 M_{00}$$



effect of Γ

→ the stronger Γ , the faster the velocities on the upper surface → pressure drop

→ pressure difference → lift force : $L = g M_{00} \Gamma$

hint: $2 \cdot \sin \varphi \cdot \cos \varphi = \sin 2\varphi$ and $-\sin 2\varphi = \sin(2(\pi - \varphi)) = \sin 2\varphi'$

$$\Rightarrow c_{pk} = \frac{\sin 2\varphi'}{\varphi'} - \left(\frac{\sin \varphi'}{\varphi'}\right)^2$$

d) isobars: $c_p = \text{const}$

$$c_p = -\frac{h}{\pi} \cdot \frac{2x + \frac{hy}{\pi}}{x^2 + y^2} \Rightarrow x^2 + y^2 = -2 \frac{h}{\pi c_p} x - \left(\frac{h}{\pi}\right)^2 \cdot \frac{1}{c_p} + \left(\frac{h}{\pi}\right)^2 \cdot \frac{1}{c_p^2} - \left(\frac{h}{\pi}\right)^2 \cdot \frac{1}{c_p^2}$$

$$\Rightarrow x^2 + 2 \frac{h}{\pi c_p} x + \left(\frac{h}{\pi}\right)^2 \cdot \frac{1}{c_p^2} + y^2 = -\frac{h^2}{\pi^2} \cdot \frac{1}{c_p} + \frac{h^2}{\pi^2} \cdot \frac{1}{c_p^2}$$

$$\Rightarrow \left(x + \frac{h}{\pi c_p}\right)^2 + y^2 = \underbrace{\left(1 - c_p\right)\left(\frac{h}{\pi c_p}\right)^2}_{R^2}$$

\Rightarrow circles around $(-\frac{h}{\pi c_p}, 0)$ with radius $\frac{h}{\pi c_p} \cdot \sqrt{1 - c_p}$

Potential theory

$$F(z) = \int \bar{w}(z) dz = \phi(x, y) + i\psi(x, y)$$

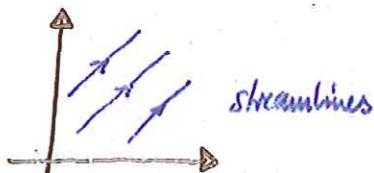
\uparrow potential function \uparrow stream function

$$\Rightarrow \bar{w} = \frac{dF}{dz} = u - iv$$

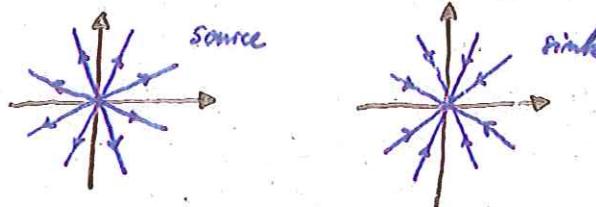
$$z = x + iy = r e^{i\varphi}$$

$$= r(\cos\varphi + i\sin\varphi)$$

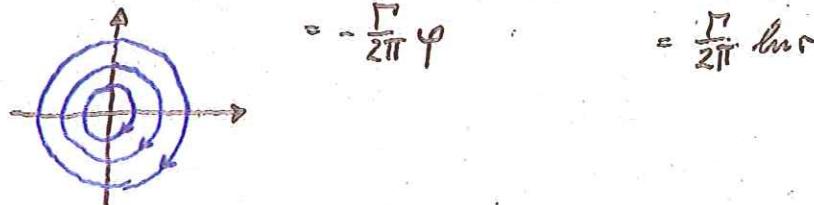
Parallel flow: $F(z) = (u_{00} - iv_{00}) \cdot z \rightarrow \phi = u_{00}x + v_{00}y ; \psi = u_{00}y - v_{00}x$



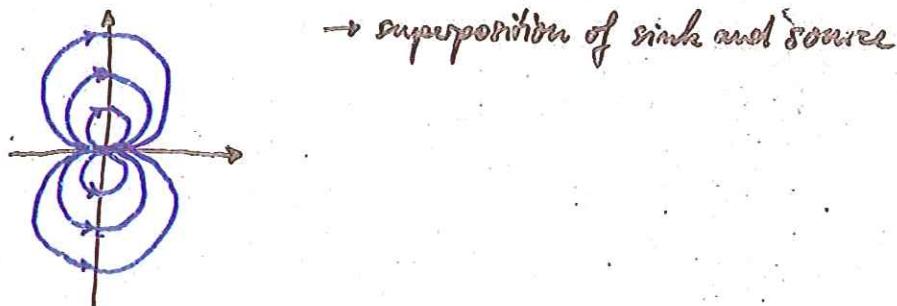
Source, sink: $F(z) = \frac{\Gamma}{2\pi} \ln z \rightarrow \phi = \frac{\Gamma}{2\pi} \ln r ; \psi = \frac{\Gamma}{2\pi} \varphi$



Vortex: $F(z) = \frac{\Gamma}{2\pi} i \ln z \rightarrow \phi = -\frac{\Gamma}{2\pi} \operatorname{arctan} \frac{y}{x} ; \psi = \frac{\Gamma}{2\pi} \ln \sqrt{x^2 + y^2}$

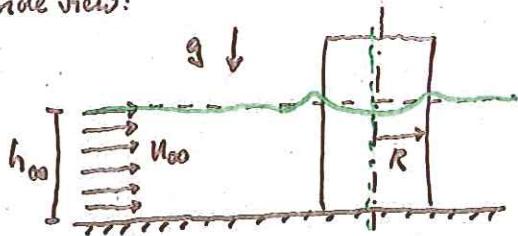


Dipole: $F(z) = \frac{M}{2\pi R} \rightarrow \phi = \frac{M}{2\pi} \frac{x}{x^2 + y^2} ; \psi = \frac{-M}{2\pi} \frac{y}{x^2 + y^2}$



Water is flowing against a bridge pier with the velocity u_{∞} . The pier has a circular cross-section. Far away from the pier the water level is h_{∞} .

side view:



$$u_{\infty} = 1 \text{ m/s}$$

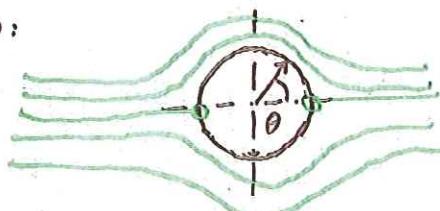
$$h_{\infty} = 6 \text{ m}$$

$$R = 2 \text{ m}$$

$$\rho = 10^3 \text{ kg/m}^3$$

$$g = 10 \text{ m/s}^2$$

top view:



a) Determine the water level at the pier as a function of θ .

b) Calculate the water level in the stagnation points.

c) Calculate the minimum water level.

circular cylinders: Dipole + parallel flow

$$\Rightarrow F(z) = u_{\infty} \cdot z + \frac{M}{2\pi z} \quad \text{with } z = r(\cos \theta + i \sin \theta)$$

$$\Rightarrow \phi = \left(u_{\infty} + \frac{M}{2\pi r^2} \right) r \cos \theta$$

$$\psi = \left(u_{\infty} - \frac{M}{2\pi r^2} \right) r \sin \theta$$

$$\begin{aligned} \text{with } \frac{1}{z} &= \frac{1}{r(\cos \theta + i \sin \theta)} \cdot \frac{r(\cos \theta - i \sin \theta)}{r(\cos \theta - i \sin \theta)} \\ &= \frac{r(\cos \theta - i \sin \theta)}{r^2} \end{aligned}$$

$$\Rightarrow v_r = \frac{\partial \phi}{\partial r} = \left(u_{\infty} - \frac{M}{2\pi r^2} \right) \cdot \cos \theta$$

$$\Rightarrow v_\theta = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = - \left(u_{\infty} + \frac{M}{2\pi r^2} \right) \cdot \sin \theta$$

symmetric flow: stagnation points at $\theta = 0$ and $\theta = \pi$ and $r = R$.

$$\Rightarrow v_r = v_\theta = 0 \Rightarrow M_{\infty} - \frac{M}{2\pi R^2} = 0 \Rightarrow M = M_{\infty} \cdot 2\pi \cdot R^2$$

$$\Rightarrow v_\theta = - \left(M_{\infty} + \frac{R^2 M_{\infty}}{r^2} \right) \cdot \sin \theta$$

On the surface of the cylinder: $v_r = 0$ and $v_\theta = -2 M_{\infty} \cdot \sin \theta$

$$\text{Bernoulli: } p_a + \rho g h_{\infty} + \frac{1}{2} M_{\infty}^2 = p_a + \rho g h(\theta) + \frac{1}{2} v^2$$

$$\rightarrow v^2 = v_{\theta, \text{surf}}^2 = 4 M_{\infty}^2 \cdot \sin^2 \theta$$

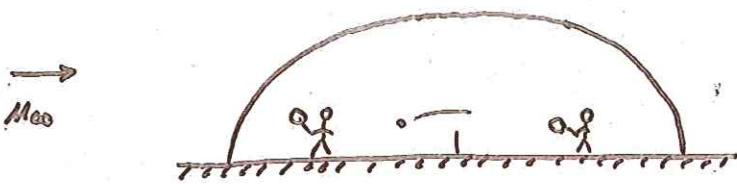
$$\Rightarrow h(\theta) = h_{\infty} + \frac{M_{\infty}^2}{2g} (1 - 4 \sin^2 \theta)$$

$$\begin{aligned} h(0, \pi) &= \\ &= h_{\infty} + \frac{M_{\infty}^2}{2g} = 6.05 \text{ m} \end{aligned}$$

$$\theta_{\min} = \frac{\pi}{2}, \frac{3\pi}{2}$$

$$\begin{aligned} h(\pi_2, \frac{3\pi}{2}) &= \\ &= h_{\infty} - \frac{3 M_{\infty}^2}{2g} = 5.85 \text{ m} \end{aligned}$$

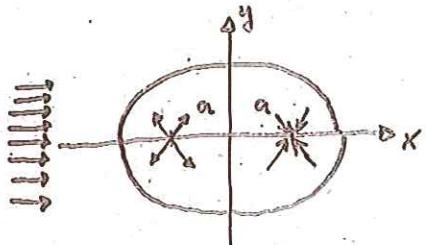
The flow around a tennis sports ball should be described by potential theory.



- What potential function should be used to describe the problem?
- Determine the velocities \$u(x,y)\$ and \$v(x,y)\$ using the complex conjugate velocity \$\bar{w}\$.
- Determine the stagnation points and the contour streamline.
- Sketch the streamlines.
- What 2 simplifications are used in potential theory according to real flows?

- a) Superposition of parallel flow, source and sink:

$$F(z) = M_{\infty} z + \frac{E}{2\pi} \ln(z+a) - \frac{E}{2\pi} \ln(z-a)$$



$$\begin{aligned} b) \bar{w} &= \frac{dF}{dz} = M - iv = M_{\infty} + \frac{E}{2\pi} \left(\frac{1}{z+a} - \frac{1}{z-a} \right) \\ &= M_{\infty} + \frac{E}{2\pi} \left(\frac{x+a-iy}{(x+a)^2+y^2} - \frac{x-a-iy}{(x-a)^2+y^2} \right) \end{aligned}$$

$$\Rightarrow M = M_{\infty} + \frac{E}{2\pi} \left(\frac{x+a}{(x+a)^2+y^2} - \frac{x-a}{(x-a)^2+y^2} \right)$$

$$V = \frac{E}{2\pi} \left(\frac{y}{(x+a)^2+y^2} - \frac{y}{(x-a)^2+y^2} \right)$$

- c) stagnation point is part of the contour stream line

s.p. \$M=V=0 \rightarrow\$ symmetry: \$y_s=0 \rightarrow v(x_s, y_s)=0\$

$$\begin{aligned} M=0 &= M_{\infty} + \frac{E}{2\pi} \left(\frac{x_s+a}{(x_s+a)^2+y_s^2} - \frac{x_s-a}{(x_s-a)^2+y_s^2} \right) = M_{\infty} + \frac{E}{2\pi} \left(\frac{1}{x_s+a} - \frac{1}{x_s-a} \right) \\ &= M_{\infty} - \frac{E}{2\pi} \left(\frac{2a}{x_s^2-a^2} \right) \quad \Rightarrow x_s = \pm \sqrt{\frac{aE}{\pi M_{\infty}}} + a \end{aligned}$$

contour stream line: $\psi(x, y) = \psi_k = \operatorname{Im}(F(z))$

$$F(z) = \phi + i\psi$$

$$= M_\infty (x+iy) + \frac{E}{2\pi} \left[\ln r_1 e^{i\varphi_1} - \ln r_2 e^{i\varphi_2} \right]$$

with: $r_1 = \sqrt{(x+a)^2 + y^2}$; $r_2 = \sqrt{(x-a)^2 + y^2}$

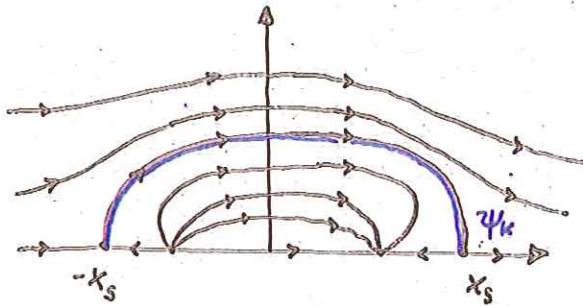
$$\varphi_1 = \arctan\left(\frac{y}{x+a}\right); \varphi_2 = \arctan\left(\frac{y}{x-a}\right)$$

$$\psi(x, y) = M_\infty y + \frac{E}{2\pi} \cdot \left(\arctan\left(\frac{y}{x+a}\right) - \arctan\left(\frac{y}{x-a}\right) \right)$$

$$\psi_k = \psi_{sp} \Rightarrow \psi_{sp}(x_s, y_s) = 0 \quad \text{since } y_s = 0$$

$$\Rightarrow 0 = M_\infty y + \frac{E}{2\pi} \cdot \left(\arctan\left(\frac{y}{x+a}\right) - \arctan\left(\frac{y}{x-a}\right) \right)$$

d) sketch:



- e) simplifications:
- contours is equal to streamlines \rightarrow no-slip condition not fulfilled
 - rotation free flow is assumed